

## DESCRIPTION

Inneos' 940nm 12 Gbps VCSEL was designed specifically for wide temperature operating environments from -55°C to +85°C to meet the needs of automotive, industrial and aerospace applications. The device allows for wirebond to the n-contact on either side of the p-contact to support a variety of driver interfaces and packaging options. The Inneos 940nm VCSEL maintains superior performance in the harshest environments.



## FEATURES

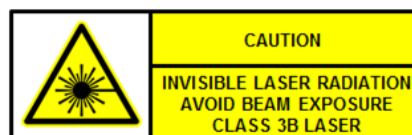
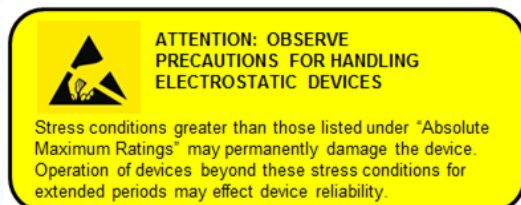
- Wide operating temperature from -55°C to +85°C
- Operation up to 12 Gbps
- Top-emitting
- Single channel

## ORDERING INFORMATION

PART NUMBER	DESCRIPTION
V940-12GWA-1TGA	12 Gbps 940 nm VCSEL, Bare Die, -55°C to 85°C, Gel-Pak

## APPLICATIONS

- Transmitter Optical Sub-Assemblies
- High-performance Transceivers
- Harsh Environment Sensors



## ABSOLUTE MAXIMUM RATINGS

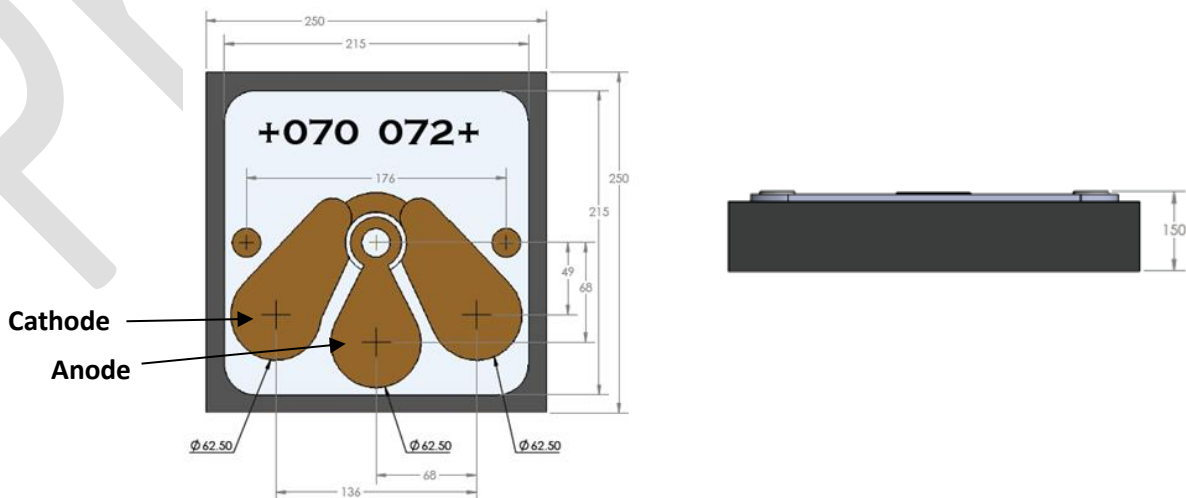
PARAMETER	SYMBOL	MIN	MAX	UNITS
Storage Temperature Range	$T_S$	-65	125	°C
Operating Temperature Range	$T_O$	-55	85	°C
Reverse Voltage	$V_R$		8	V
Continuous Forward Current	$I_F$		10	mA
ESD Protection (HBM)			200	V

## OPTICAL/ELECTRICAL SPECIFICATIONS

PARAMETER	CONDITIONS	SYMBOL	UNITS	MIN	TYPICAL	MAX
Emission Wavelength	T <sub>o</sub> =30°C @ 6mA	$\lambda_c$	nm	930	940	950
Variation of Wavelength with Temperature	-	$\frac{\Delta\lambda}{\Delta T}$	nm/°C	-	0.07	-
Spectral Width <sup>a</sup>	T <sub>o</sub> =-55°C @ 6mA	$\sigma_\lambda$	nm	-	-	1.00
	T <sub>o</sub> =85°C @ 6mA					
Threshold Current <sup>b</sup>	T <sub>o</sub> =-55°C, 85°C	$I_{th}$	mA	-	-	1.5
	T <sub>o</sub> =30°C			-	0.75	-
Average Operating Current		$I_{avg}$	mA	-	6	-
Operating Voltage	T <sub>o</sub> =-55°C @ 6mA	$V_o$	V	-	-	2.8
	T <sub>o</sub> =85°C @ 6mA			-	2.2	-
Optical Output Power	T <sub>o</sub> =-55°C, 85°C @ 6mA	$P_o$	mW	1.0	-	-
	T <sub>o</sub> =30°C @ 6mA			-	2.5	-
Small Signal Bandwidth <sup>c</sup>	T <sub>o</sub> =85°C @ 6mA	$f_{3dB}$	GHz	9.0	-	-
Relative Intensity Noise <sup>d</sup>	T <sub>o</sub> =85°C @ 6mA	$RIN_{12}$	dB/Hz	-	-	-128
Beam Divergence Half Angle (1/e <sup>2</sup> ) <sup>e</sup>	T <sub>o</sub> =30°C @ 6mA	$\theta_{1/2}$	deg	-	15	-
Slope Efficiency <sup>f</sup>	T <sub>o</sub> =-55°C	$SE$	mW/mA	-	0.6	-
	T <sub>o</sub> =85°C			-	0.3	-
Differential Resistance <sup>g</sup>	T <sub>o</sub> =-55°C @ 6mA	$R_{diff}$	$\Omega$	-	75	-
	T <sub>o</sub> =85°C @ 6mA			-	60	-

## MECHANICAL OUTLINE

Dimensions are in microns.



## PARAMETER CALCULATION METHODS USED

a. Spectral width is calculated based on FOTP-127 where the spectral level of the measured spectra below 20dB from maximum value are made zero and RMS spectral width is calculated based on formula

$$\Delta\lambda_{RMS} = \sqrt{\frac{\sum_{i=1}^N P_i \lambda_i^2}{\sum_{i=1}^N P_i} - \left(\frac{\sum_{i=1}^N P_i \lambda_i}{\sum_{i=1}^N P_i}\right)^2}$$

where ' $\lambda_i$ ' is the wavelength and ' $P_i$ ' is the optical power level of the  $i$ th point in the spectra.

b. The threshold current is derived by a linear fit method using 10% and 20% of peak optical power points. Threshold current is the point at which the optical power is zero using the linear fit.

c. The small signal bandwidth is obtained from optical response measurements at set current and reading the cut off frequency at which the power level is 3dB down from the power level at DC.

d. Relative intensity noise:  $RIN_{12}$  is the DC-RIN measured with -12dB return. The DC-RIN is measured using an electrical spectrum analyzer with resolution bandwidth set to 1MHz, calibrated photodetector and broad-band amplifiers. The RIN per unit bandwidth is calculated using the formula,

$$RIN \left(\frac{dB}{Hz}\right) = RIN [dBm] - 10\log_{10}(I_p^2 R_m) [dBm] - A [dB] - 10\log_{10}(\Delta f [GHz])$$

where 'RIN' is the peak RIN on electrical spectrum analyzer with resolution bandwidth ' $\Delta f$ ', ' $I_p$ ' is the measured photocurrent, ' $R_m$ ' is the input resistance of measurement system, and 'A' is the amplification.

e. Beam divergence half-angle is derived from measurement of optical power in far-field at various angles. The half-angle is the angular deviation from center where the power reduces by '1/e'.

f. The slope efficiency is derived by linear fit method using 10% and 20% of peak optical power points. Slope efficiency is the slope of the lineal fit of optical power and drive current.

g. Differential resistance at point 'i' of the measured LIV is calculated based on formula,

$$R_{diff} = \frac{V_i - V_{i-1}}{I_i - I_{i-1}}$$

where ' $V_i$ ', ' $V_{i-1}$ ' are the measured voltages at set currents ' $I_i$ ' and ' $I_{i-1}$ ' respectively.